

# Measurement of Rain Attenuation in Terahertz Wave Range

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## ABSTRACT

Rain attenuation at 355.2 GHz in the terahertz wave range was measured with our new 355.2 GHz measuring system under rainfall intensities up to 25 mm/hr. Rain attenuation coefficients were also calculated using four raindrop-size distributions, the Marshall-Palmer (M-P), Best, Polyakova-Shifrin (P-S) and Weibull distributions, and using a specific rain attenuation model for prediction methods recommended by ITU-R. Measurements of a terahertz wave taken at 355.2 GHz were compared with our calculations. Results showed that the propagation experiment was in very good agreement with a calculation from a specific attenuation model for use in prediction method recommended by ITU-R.

**Keywords:** Terahertz Wave, Rain Attenuation, Raindrop-Size Distribution, M-P Distribution, Weibull Distribution, ITU-R

## 1. Introduction

Recent advances in electronic and electro-optical terahertz devices, and improvements in system technology, have stimulated in imaging and sensing applications in the security and non-destructive testing fields [1].

Rain attenuation is one of the most serious obstacles to overcome for imaging and sensing systems to detect hazardous things using a terahertz waves above 300 GHz because of its masking action. Raindrop-size distributions have been found to play an important role in monitoring rainfall and in predicting rain attenuation. Rain attenuation is particularly severe and greatly dependent on various models of raindrop-size distribution in millimeter- and terahertz-wave systems.

## 2. Measuring Rain Attenuation

### 2.1. Measuring System

Experimental data were collected at 355.2 GHz by using the terahertz wave propagation measuring system shown in **Figure 2**. A summary of the system parameters is given in **Table 1**, and a photograph of the transmitter and detector are shown in **Figure 1**.

**Figure 2** outlines our new system for measuring rain attenuation in terahertz wave range. The system consists of a transmitter, detector, interface, rain-intensity gauge, and ancillary devices such as a thermometer and data-

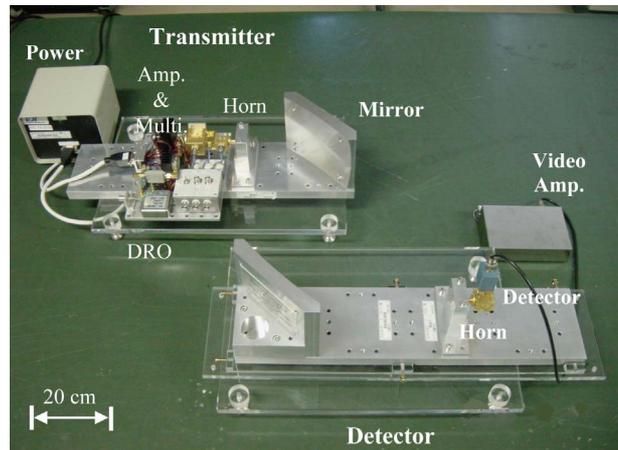
logger/controller. The transmitter and detector use a corrugated conical horn feeding an off-axis elliptical mirror to collimate beams, yielding a directivity of 50 dB. The transmitter has approximately +8 dBm of output power at terahertz wave range, and was pulse modulated at 12 kHz using a transistor-transistor logic (TTL) signal. To cope with the fluctuation in detection sensitivity due to temperature variation, a correction was applied to the detected voltage, based on previous measurements of the detector's thermal characteristics. The measurement level stability after thermal linear correction was within 0.1 dB.

The terahertz wave transmitter is driven by a phase locked oscillator (PLO), which is oscillated by the dielectric resonant oscillator (DRO) and locked to the 100 MHz of the reference oscillator. The PLO output is then quadrupled and then amplified using a monolithic microwave integrated circuit (MMIC) amplifier to a power level of approximately 1 W. A cascade of three varactor frequency doublers (VFDs) are used to convert the amplifier output to 355.2 GHz. The output power is adjusted to keep the detector in square law using a rubber plate as an attenuator.

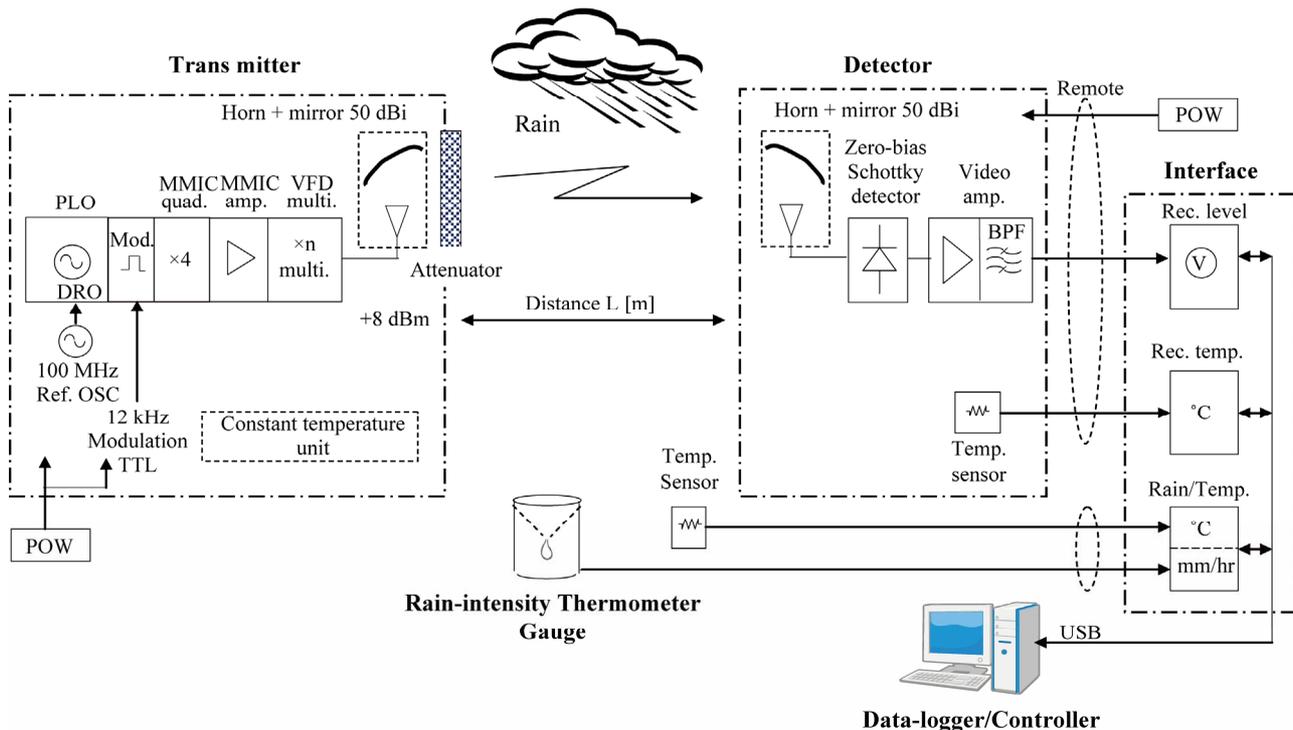
The propagated terahertz wave signal is received using a zero-bias Schottky diode detector, and the output voltage is amplified using a low-noise video amplifier followed by a 12-kHz band pass filter (BPF) to reduce the

**Table 1. Summary of the instrumentation system parameters.**

Item	Transmitter	Detector	Measure
frequency	355.2 GHz	330 to 500 GHz	-
output level	+8 dBm	-	-
receiving level	-	-20 to -55 dBm	-
antenna gain (horn + mirror)	50 dBi	-	-
polarization	horizontal	-	-
Rain-fall rate range	-	-	0 to 100 mm/hr
operation temperature	-	5°C to 40°C	-



**Figure 1. Photograph of transmitter and detector.**



**Figure 2. Terahertz wave propagation measuring system.**

noise bandwidth. The system collects the data on the receiving level, temperature, and rainfall rate, which are then digitized using an analog-to-digital (A/D) converter. The data logger/controller controls all devices and collects and stores the data, and measuring parameters.

**2.2. Measuring System Stability**

Prior to the measuring rain attenuation, a system stability check was carried out under the same conditions as those for measurement. **Figure 3** shows the received out put level at the video amplifier and corresponding ambient

temperature and temperature of the detector plotted as a function of time for a 24-hours period from 19:14 on 24<sup>th</sup> April to 19:14 on 25<sup>th</sup> April. The wind speed and direction during the checking period near the measurement area were 2 to 5 m/s and NNE or SSE, and the weather was mostly sunny. The measuring time interval was one minute.

**2.3. Measuring Rain Attenuation**

Measurement was carried out at the National Defense Academy in Yokosuka City, Japan during March and

April 2010. The propagation range was 33 m. **Figure 3** shows the change attenuation coefficient at 355.2 GHz and the corresponding rain rate plotted as a function of time for one event, on 28 April, from 10:00 to 16:00, during that period. The wind speed and direction during the measurement period near the measurement area were 6 to 7 m/s and N or NNW. Temperature is shown in **Figure 4**. The measuring time interval was one minute, depending on the required accumulation time for the rain gauge.

Between 10:00 to 16:00, as shown in **Figure 4**, the rain could be characterized as widespread. The attenuation for this period corresponds to the rain rates in **Figure 4**.

### 3. Calculations

Rain attenuation was calculated by using four types of raindrop-size distributions and a specific attenuation model for use in the prediction method recommended by ITU-R.

#### 3.1. Raindrop-Size Distributions

Marshall and Palmer [2] proposed the following well-known empirical expression by fitting their data and the Laws and Parsons data. Their data was taken in Ottawa, Canada in 1946 using the filter paper method. The fit of this distribution to the experimental points was not very good for drops less than  $D = 1$  mm.

$$\begin{aligned} N(D) &= N_0 e^{-\Lambda D} \\ N_0 &= 8000 \text{ m}^{-3} \text{ mm}^{-1} \\ \Lambda &= 4.1 R^{-0.21} \text{ mm}^{-1} \end{aligned} \quad (1)$$

where  $D$  is the diameter in mm, and  $R$  is the precipitation rate in mm/hr.

Best [3] proposed a drop-size distribution model after analyzing a large amount of experimental data in 1950. This is written as:

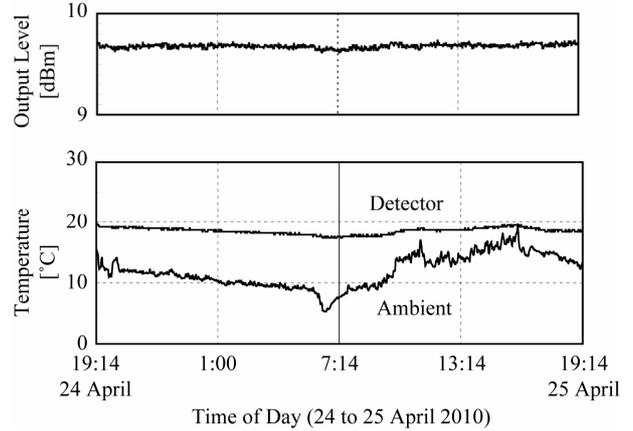
$$\begin{aligned} N(D) &= \frac{13.5W}{\pi a^4} \left(\frac{D}{a}\right)^{-1.75} e^{-\left(\frac{D}{a}\right)^{2.25}} \\ W &= 8000 R^{0.846} \text{ m}^{-3} \text{ mm}^3 \\ a &= 1.3 R^{0.232} \text{ mm} \end{aligned} \quad (2)$$

Litvinov proposed a model [4] in 1957 and [5] in 1958 due to Polyakva and Shifrin (P-S) using the Russian data for all three types of rain. This model was also described by Krasnyuk, Rozenberg and Chistyakov [6] in 1968 and by University of Tennessee [7] in 1975. It was one case of Gamma distribution proposed by Atlas and Ulbrich [8] in 1984:

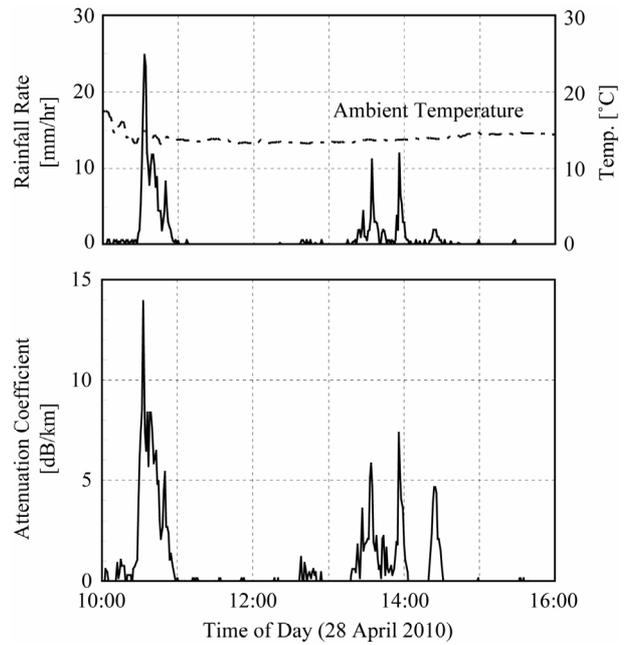
$$N(D) = N_0 D^2 e^{-\Lambda D} \quad (3)$$

$N_0$  and  $\Lambda$  vary based on the rain types of thawing are shown in **Table 2**.

Sekine and Lind [9] proposed a Weibull distribution in 1982 by using the FOA data (from the National Defence Research Institute) in Sweden:



**Figure 3.** Received output level of video amp. and ambient temperature.



**Figure 4.** Attenuation coefficient at 355.2 GHz and corresponding rainfall rate.

**Table 2.** Values for  $N_0$  and  $\Lambda$ .

Type of rain	$N_0 \text{ m}^{-3} \text{ mm}^{-1}$	$\Lambda \text{ mm}^{-1}$
Thawing of Pellets (Hail)	$64500 R^{-0.5}$	$6.95 R^{-0.27}$
Thawing of Granular Snow (Sleet)	$11750 R^{-0.29}$	$4.87 R^{-0.2}$
Thawing of Non Granular Snow (Sleet)	$2820 R^{-0.18}$	$4.01 R^{-0.19}$

$$\begin{aligned}
 N(D) &= N_0 \frac{c}{b} \left(\frac{D}{b}\right)^{c-1} e^{-\left(\frac{D}{b}\right)^c} \\
 N_0 &= 1000 \text{ m}^{-3} \\
 b &= 0.26 R^{0.44} \text{ mm} \\
 c &= 0.95 R^{0.14}
 \end{aligned}
 \tag{4}$$

This distribution is retained for microwave and terahertz applications [10-23].

### 3.2. Calculations of Rain Attenuation

For calculations using by raindrop-size distributions, rain specific attenuation  $A$  in dB/km is calculated by integrating all of the drop sizes as

$$A = 4.343 \int Q(D, \lambda, m) N(D) dD \tag{5}$$

where  $Q$  is the attenuation cross section which is a function of the drop diameter  $D$ , the wavelength of the radio wave  $\lambda$ , and the complex refractive index of the water drop  $m$ , which is a function of the frequency and the temperature, and  $N(D)$  is the drop-size distribution.

The attenuation cross section  $Q$  is found by applying the classical Mie scattering theory for a plane wave radiation to an absorbing sphere particle. According to Hulst [24], the cross section  $Q$  is expanded as

$$Q(D, \lambda, m) = \frac{\lambda^2}{2\pi} \sum_{n=1}^{\infty} (2n+1) \text{Re}[a_n + b_n] \tag{6}$$

where  $a_n$  and  $b_n$  are the Mie scattering coefficients, which are complex functions of  $m$ ,  $D$  and  $\lambda$ . The ‘‘Mie scattering coefficients’’  $a_n$  and  $b_n$  in Equation (6) represent the contribution to the scattered field from the multi poles induced in a sphere, such as a raindrop. The complex refractive index of liquid water  $m$  was taken from Ray’s research [25].

For calculation by using the recommended prediction methods by ITU-R [26], rain specific attenuation  $\gamma_R$  dB/km is obtained from the rain rate  $R$  mm/hr using the power-law relationship:

$$\gamma_R = kR^\alpha \tag{7}$$

The constant values for the constants for the coefficients  $k$  and  $\alpha$  are determined as functions of frequency,  $f$  GHz, in the range from 1 to 1000 GHz, from the equations which have been developed from curve-fitting to power-law coefficients derived from scattering calculations. This is shown in ITU-R P.838-3 [26]. This calculation was carried out with a flat path elevation angle and the horizontal polarization of radiation because the experiments were conducted in a flat area. Also from our tentative calculation, variation of rain attenuation was less than 0.1 dB/km for each vertical, horizontal, and circular

polarization at 355.2 GHz under a rainfall rate of up to 25 mm/hr.

### 3.3. Experiments and Computations

Figure 5 shows the results of experiments and computations for 355.2 GHz under a rainfall rate of up to 25 mm/hr. For the calculations of rain attenuation, the Marshall and Palmer (M-P), Best, Polyakva and Shifrin (P-S), and Weibull rain drop-size distributions, described in Equations (1)-(4), respectively, were used, and a specific attenuation model recommended by ITU-R was used for ITU-R described in Equation (7).

An experimental fit curve (shown by the broken line), derived using the aid of the least squares method from the raw data (triangles in Figure 5) is described as  $A = 1.79 R^{0.58}$ .

The experimental data was compared with the calculations. The deviation of the empirical data and the calculated attenuation coefficients were estimated by calculating the root mean square error (RMSE). The results are shown in Table 3. Results showed that the calculations from Weibull and ITU-R were in good agreement with the experimental data. The best fit was the calculation from ITU-R with the smallest RMSE.

### 4. Conclusions

Rain attenuation at 355.2 GHz was measured at the National Defense Academy and calculated using four raindrop-size distributions and an ITU-R specific attenuation

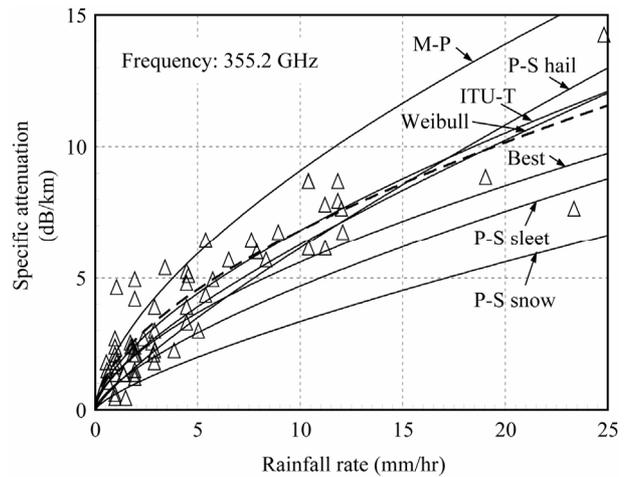


Figure 5. Comparison between calculations and measurements at 355.2 GHz.

Table 3. RMSE values for attenuation coefficients.

Calculations	ITU-R	Weibull	M-P	Best	P-S hail	P-S sleet	P-S snow
RMSE	0.26	0.43	2.81	1.32	0.80	2.20	3.71

model. The calculated results were compared with propagation experiments under rainfall intensities of up to 25 mm/hr. The propagation experimental results were in very good agreement with of the calculation from the specific attenuation model for use in prediction method recommended by ITU-R provided the best fit for the experimental data. Finally, there is greater interest in the rain attenuation at terahertz wave range. An experiment on rain attenuation above 300 GHz at different rainfall rates with various raindrop-size distributions is needed, especially at a higher rainfall rate that may cause fatally damage terahertz applications.

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